

TITLE OF THE INVENTION

5 BACKGROUND OF THE INVENTION

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temperature.

~~In the case where a gas having a high negativity,~~
i.e., a gas that tends to generate negative ions, such as
 Cl_2 , SF_6 , is formed into plasma, when the electron
5 temperature becomes about 3 eV or lower, larger amounts of
negative ions are generated than with higher electron
temperatures. Taking advantage of this phenomenon makes it
possible to prevent etching configuration abnormalities,
so-called notch, which may occur when positive charges are
10 accumulated at the bottom of micro-patterns due to
excessive incidence of positive ions. This allows etching
of extremely micro patterns to be achieved with high
precision.

Also, in the case where a gas containing carbon
15 and fluorine, such as C_xF_y or $\text{C}_x\text{H}_y\text{F}_z$ (where x , y , z are
natural numbers), which is generally used for etching of
insulating films such as silicon oxide, is formed into
plasma, when the electron temperature becomes about 3 eV or
lower, gas dissociation is suppressed more than with higher
20 electron temperatures, where, in particular, generation of
F atoms, F radicals and the like is suppressed. Because F
atoms, F radicals and the like are higher in the rate of
silicon etching, insulating film etching can be carried out
at larger selection ratios to silicon etching the more with
25 lower electron temperatures.

Also, when the electron temperature becomes 3 eV or lower, ion temperature and plasma potential also becomes lower, so that ion damage to the substrate in plasma CVD can be reduced.

5 As a technique capable of generating plasma having low electron temperature, plasma sources using high-frequency power of VHF band or UHF band are now receiving attention.

Fig. 15 is a sectional view of a dual-frequency excitation parallel-flat plate type plasma processing apparatus. Referring to Fig. 15, while interior of a vacuum chamber 201 is maintained to a specified pressure by introducing a specified gas from a gas supply unit 202 into the vacuum chamber 201 and simultaneously performing evacuation by a pump 203 as an evacuating device, a high-frequency power of 100 MHz is supplied to a counter electrode 205 by a counter-electrode-use-high-frequency power supply 204. Then, plasma is generated in the vacuum chamber 201, where plasma processing such as etching, deposition, and surface reforming can be carried out on a substrate 207 placed on a substrate electrode 206. In this case, as shown in Fig. 15, by supplying high-frequency power also to the substrate electrode 206 by a substrate-electrode-use-high-frequency power supply 208, ion energy that reaches the substrate 207 can be controlled. In

addition, the counter electrode 205 is insulated from the vacuum chamber 201 by an insulating ring 211.

Fig. 16 is a sectional view of a plasma processing apparatus which we have already proposed and which has an antenna type plasma source mounted thereon. Referring to Fig. 16, while interior of a vacuum chamber 301 is maintained to a specified pressure by introducing a specified gas from a gas supply unit 302 into the vacuum chamber 301 and simultaneously performing evacuation by a pump 303 as an evacuating device, a high-frequency power of 100 MHz is supplied to a spiral antenna 313 on a dielectric window 314 by an antenna-use-high-frequency power supply 312. Then, plasma is generated in the vacuum chamber 301 by electromagnetic waves radiated into the vacuum chamber 301, where plasma processing such as etching, deposition, and surface reforming can be carried out on a substrate 307 placed on a substrate electrode 306. In this case, as shown in Fig. 16, by supplying high-frequency power also to the substrate electrode 306 by a substrate-electrode-use-high-frequency power supply 308, ion energy that reaches the substrate 307 can be controlled.

However, there has been an issue that the conventional methods shown in Figs. 15 and 16 have difficulty in obtaining uniformity of plasma.

Fig. 17 shows results of measuring ion saturation

current density at a position 20 mm just above the
substrate 207 in the plasma processing apparatus of Fig. 15.

Conditions for plasma generation are gas type of Cl_2 and
gas flow rate of 100 sccm, a pressure of 1 Pa, and a high-
frequency power of 2 kW. It can be understood from Fig. 17
that plasma density is higher in peripheral regions.

Fig. 18 shows results of measuring ion saturation
current density at a position 20 mm just above the
substrate 307 in the plasma processing apparatus of Fig. 16.
Conditions for plasma generation are gas type of Cl_2 and
gas flow rate of 100 sccm, a pressure of 1 Pa, and a high-
frequency power of 2 kW. It can be understood from Fig. 18
that plasma density is higher in peripheral regions.

Such nonuniformity of plasma is phenomenon that
could not be seen with the frequency of the high-frequency
power of 50 MHz or less. Whereas the 50 MHz or higher
high-frequency power needs to be used in order to lower the
electron temperature of plasma, there are produced, in this
frequency band, not only an advantage that plasma is
generated by the counter electrode or antenna being
capacitively or inductively coupled to the plasma, but also
an advantage that plasma is generated by electromagnetic
waves, which are radiated from the counter electrode or
antenna, propagating on the surface of the plasma. In
peripheral regions of the vacuum chamber, which serve as

reflecting surfaces for the electromagnetic waves that have propagated on the surface of the plasma, stronger electric fields are developed so that thick plasma is generated.

Also, as described above, in the case where a gas having a high negativity, i.e., a gas that tends to generate negative ions, such as Cl_2 , SF_6 , is formed into plasma, when the electron temperature becomes about 3 eV or lower, larger amounts of negative ions are generated than with higher electron temperatures. Taking advantage of this phenomenon makes it possible to prevent a phenomenon that perpendicularity of the incident angle of ions onto the substrate worsens when positive charges are accumulated at the bottom of micro-patterns due to excessive incidence of positive ions. This allows etching of extremely micro patterns to be achieved with high precision. Besides, that is an expectation for process improvement making use of the high reactivity of negative ions.

Also, in the case where a gas containing carbon and fluorine, such as C_xF_y or $\text{C}_x\text{H}_y\text{F}_z$ (where x , y , z are natural numbers), which is generally used for etching of insulating films such as silicon oxide, is formed into plasma, when the electron temperature becomes about 3 eV or lower, gas dissociation is suppressed more than with higher electron temperatures, where, in particular, generation of F atoms, F radicals and the like is suppressed. Because F

atoms, F radicals and the like are higher in the rate of
~~silicon etching, insulating film etching can be carried out~~
at larger selection ratios to silicon etching the more with
lower electron temperatures.

5 Also, when the electron temperature becomes 3 eV
or lower, ion temperature and plasma potential also become
lower, so that ion damage to the substrate in plasma CVD
can be reduced.

10 It is plasma sources using high-frequency power
of VHF band that is currently receiving attention as a
technique capable of generating plasma low in electron
temperature and capable of generating plasma superior in
ignitability.

15 Fig. 24 is a sectional view of a dual-frequency
excitation parallel-flat plate type plasma processing
apparatus. Referring to Fig. 24, while interior of a
vacuum chamber 401 is maintained to a specified pressure by
introducing a specified gas from a gas supply unit 402 into
the vacuum chamber 401 and simultaneously performing
20 evacuation by a pump 403 as an evacuating device, a high-
frequency power of 100 MHz is supplied to a counter
electrode 407 via a matching box 405 and a high-frequency
coupling device (mount) 406 by a counter-electrode-use-
high-frequency power supply 404. Then, plasma is generated
25 in the vacuum chamber 401, where plasma processing such as

etching, deposition, and surface reforming can be carried
out on a substrate 409 placed on a substrate-electrode 408.

In this case, as shown in Fig. 24, by supplying high-frequency power also to the substrate electrode 408 by a
5 substrate-electrode-use-high-frequency power supply 410,
ion energy that reaches the substrate 409 can be controlled.
In addition, the counter electrode 407 is insulated from
the vacuum chamber 401 by an insulating ring 411. The
matching box 405 comprises a high-frequency input terminal
10 412, a first variable capacitor 413, a high-frequency
output terminal 414, a second variable capacitor 415, a
first motor 416, a second motor 417, and a motor control
circuit 418.

However, there has been an issue that the
15 conventional method shown in Fig. 24 has difficulty in
obtaining uniformity of plasma.

Fig. 25 shows results of measuring ion saturation
current density at a position 20 mm just above the
substrate 409 in the plasma processing apparatus of Fig. 24.
20 Conditions for plasma generation are gas type of Cl_2 and
gas flow rate of 100 sccm, a pressure of 2 Pa and a high-
frequency power of 1 kW. Also, as shown in Fig. 24, the
second variable capacitor 415 is disposed on one side of
the measuring position in Fig. 25. It can be understood
25 from Fig. 25 that plasma density is higher on one side of

the measuring position, i.e., just below the second
variable capacitor 415.

Such nonuniformity of plasma is phenomenon that
could not be seen with the frequency of the high-frequency
power of 50 MHz or less. Whereas the 50 MHz or higher
high-frequency power needs to be used in order to lower the
electron temperature of plasma, there develops, in this
frequency band, a potential distribution in the counter
electrode 407. It can be deduced that this potential
distribution, affected by the placement of the second
variable capacitor 415 within the matching box 405, acts to
strengthen the electric fields just below the second
variable capacitor 415, resulting in nonuniformity of
plasma.

Such a phenomenon could be seen with such an
arrangement as shown in Fig. 26 in which a spiral antenna
420 is used instead of the counter electrode 407. In the
prior art example shown in Fig. 26, a dielectric window 421
is used.

SUMMARY OF THE INVENTION

In view of these issues of the prior art, an
object of the present invention is to provide plasma
processing method and apparatus, as well as a matching box
for plasma processing apparatus, capable of generating
uniform plasma.

In order to achieve the above object, the present invention has the following constitutions.

In accomplishing these and other aspects, according to a first aspect of the present invention, there is provided a plasma processing method for generating plasma within a vacuum chamber and processing a substrate placed on a substrate electrode within the vacuum chamber, the method comprising:

generating the plasma by supplying a high-frequency power having a frequency of 50 MHz to 3 GHz to a counter electrode provided opposite to the substrate while interior of the vacuum chamber is controlled to a specified pressure by introducing gas into the vacuum chamber and, simultaneously therewith, evacuating the interior of the vacuum chamber; and

processing the substrate by using the generated plasma while plasma distribution of the plasma on the substrate is controlled by an annular, groove-like plasma trap provided opposite to the substrate.

According to a second aspect of the present invention, there is provided a plasma processing method for generating plasma within a vacuum chamber and processing a substrate placed on a substrate electrode within the vacuum chamber, the method comprising:

generating the plasma by radiating electromagnetic

~~provided opposite to the substrate by supplying a high~~

5 to a specified pressure by introducing gas into the vacuum chamber and, simultaneously therewith, evacuating the interior of the vacuum chamber; and

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according to the first aspect, wherein the substrate is
~~processed while the plasma has a groove depth of not less~~
than 5 mm.

According to a sixth aspect of the present
5 invention, there is provided a plasma processing method
according to the first aspect, wherein the substrate is
processed while the plasma trap is provided in the counter
electrode.

According to a seventh aspect of the present
10 invention, there is provided a plasma processing method
according to the first aspect, wherein the plasma is
generated while the plasma trap is provided outside an
insulating ring for insulating the vacuum chamber and the
counter electrode from each other.

According to an eighth aspect of the present
15 invention, there is provided a plasma processing method
according to the first aspect, wherein the plasma is
generated while the plasma trap is provided between the
counter electrode and an insulating ring for insulating the
20 vacuum chamber and the counter electrode from each other.

According to a ninth aspect of the present
invention, there is provided a plasma processing method
according to the first aspect, wherein the plasma is
generated while the plasma trap is provided between the
25 vacuum chamber and an insulating ring for insulating the

vacuum chamber and the counter electrode from each other.

~~According to a 10th aspect of the present~~
invention, there is provided a plasma processing method
according to the second aspect, wherein the plasma is
5 generated while the plasma trap is provided in the
dielectric window.

According to an 11th aspect of the present
invention, there is provided a plasma processing method
according to the second aspect, wherein the plasma is
10 generated while the plasma trap is provided outside the
dielectric window.

According to a 12th aspect of the present
invention, there is provided a plasma processing method
according to the second aspect, wherein the plasma is
15 generated while the plasma trap is provided between the
vacuum chamber and the dielectric window.

According to a 13th aspect of the present
invention, there is provided a plasma processing method
according to the first aspect, wherein the plasma is
20 generated while DC magnetic fields are absent within the
vacuum chamber.

According to a 14th aspect of the present
invention, there is provided a plasma processing apparatus
comprising:

25 a vacuum chamber;

a gas supply unit for supplying gas into the vacuum chamber;

an evacuating device for evacuating interior of the vacuum chamber;

5 a substrate electrode for placing thereon a substrate within the vacuum chamber;

a counter electrode provided opposite to the substrate electrode;

10 a high-frequency power supply capable of supplying a high-frequency power having a frequency of 50 MHz to 3 GHz to the counter electrode; and

an annular, groove-like plasma trap provided opposite to the substrate.

15 According to a 15th aspect of the present invention, there is provided a plasma processing apparatus comprising:

a vacuum chamber;

a gas supply unit for supplying gas into the vacuum chamber;

20 an evacuating device for evacuating interior of the vacuum chamber;

a substrate electrode for placing thereon a substrate within the vacuum chamber;

25 a dielectric window provided opposite to the substrate electrode;

an antenna for radiating electromagnetic waves
~~into the vacuum chamber via the dielectric window;~~

high-frequency power supply capable of supplying
a high-frequency power having a frequency of 50 MHz to 3
5 GHz to the antenna; and

an annular, groove-like plasma trap provided
opposite to the substrate.

According to a 16th aspect of the present
invention, there is provided a plasma processing apparatus
10 according to the 14th aspect, wherein a portion surrounded
by the plasma trap out of a surface forming an inner wall
surface of the vacuum chamber and opposing the substrate has
an area 0.5 to 2.5 times that of the substrate.

According to a 17th aspect of the present
15 invention, there is provided a plasma processing apparatus
according to the 14th aspect, wherein the plasma trap has a
groove width of 3 mm to 50 mm.

According to a 18th aspect of the present
invention, there is provided a plasma processing apparatus
20 according to the 14th or 15th aspect, wherein the plasma
has a groove depth of not less than 5 mm.

According to a 19th aspect of the present
invention, there is provided a plasma processing apparatus
according to the 14th aspect, wherein the plasma trap is
25 provided in the counter electrode.

According to a 20th aspect of the present invention, ~~there is provided a plasma processing apparatus~~ according to the 14th aspect, wherein the plasma trap is provided in an insulating ring for insulating the vacuum chamber and the counter electrode from each other.

According to a 21st aspect of the present invention, there is provided a plasma processing apparatus according to the 14th aspect, wherein the plasma trap is provided outside an insulating ring for insulating the vacuum chamber and the counter electrode from each other.

According to a 22nd aspect of the present invention, there is provided a plasma processing apparatus according to the 14th aspect, wherein the plasma trap is provided between the counter electrode and an insulating ring for insulating the vacuum chamber and the counter electrode from each other.

According to a 23rd aspect of the present invention, there is provided a plasma processing apparatus according to the 14th aspect, wherein the plasma trap is provided between the vacuum chamber and an insulating ring for insulating the vacuum chamber and the counter electrode from each other.

According to a 24th aspect of the present invention, there is provided a plasma processing apparatus according to the 15th aspect, wherein the plasma trap is

provided in the dielectric window.

According to a 25th aspect of the present invention, there is provided a plasma processing apparatus according to the 15th aspect, wherein the plasma trap is
5 provided outside the dielectric window.

According to a 26th aspect of the present invention, there is provided a plasma processing apparatus according to the 15th aspect, wherein the plasma trap is provided between the vacuum chamber and the dielectric
10 window.

According to a 27th aspect of the present invention, there is provided a plasma processing apparatus according to the 14th aspect, wherein no coil or permanent magnet for applying DC magnetic fields is provided within
15 the vacuum chamber.

According to a 28th aspect of the present invention, there is provided a plasma processing apparatus according to the first aspect, further comprising a matching box for use in the plasma processing apparatus and
20 for taking impedance matching in supplying high-frequency power to a load, the matching box comprising:

a high-frequency input terminal;

a first reactive element having one end connected to the high-frequency input terminal and the other end
25 connected to a matching box casing;

wherein the second reactive element and the high-frequency output terminal are so arranged that the second

reactive element is located on a straight line passing

According to a 31st aspect of the present invention, there is provided a matching box for a plasma processing apparatus according to the 30th aspect, wherein the second reactive element and the high-frequency output terminal are so arranged that a straight line passing through a center axis of the second reactive element and a straight line passing through the center axis of the high-frequency output terminal are generally coincident with each other.

According to a 32nd aspect of the present invention, there is provided a matching box for a plasma processing apparatus according to the 30th aspect, wherein the first reactive element and the second reactive element are capacitors, respectively.

According to a 33rd aspect of the present invention, there is provided a matching box for a plasma processing apparatus according to the 30th aspect, wherein the first reactive element and the second reactive element are so arranged that a straight line passing through a center axis of the second reactive element and a straight

line passing through a center axis of the first reactive element are generally coincident with each other.

According to a 34th aspect of the present invention, there is provided a matching box for a plasma processing apparatus according to the 30th aspect, wherein the high-frequency output terminal is the other end itself of the second reactive element.

According to a 35th aspect of the present invention, there is provided a plasma processing method for generating plasma within a vacuum chamber and processing a substrate placed on a substrate electrode within the vacuum chamber, the method comprising:

so arranging a straight line passing through a center axis of the high-frequency coupling device, a straight line passing through a center axis of the counter electrode or antenna, and a straight line passing through a center axis of the substrate as to be generally coincident together;

controlling interior of the vacuum chamber to a specified pressure by introducing a gas into the vacuum chamber and, simultaneously therewith, exhausting the interior of the vacuum chamber;

generating the plasma by applying a high-frequency power having a frequency of 50 MHz to 300 MHz to a counter electrode or antenna provided opposite to the

substrate via the matching box as defined in the 30th aspect and a high-frequency coupling device provided to connect a high-frequency output terminal of the matching box and the counter electrode or antenna to each other: and

5 processing the substrate by using the generated plasma.

According to a 36th aspect of the present invention, there is provided a plasma processing method according to the 35th aspect, further comprising: before
10 controlling the interior of the vacuum chamber to the specified pressure,

so arranging a straight line passing through a center axis of the high-frequency output terminal and a straight line passing through the center axis of the high-frequency coupling device as to be generally coincident with
15 each other,

wherein the plasma is generated with the straight line passing through the center axis of the high-frequency output terminal and the straight line passing through the
20 center axis of the high-frequency coupling device being generally coincident with each other.

According to a 37th aspect of the present invention, there is provided a plasma processing method according to the 35th aspect, further comprising: before
25 controlling the interior of the vacuum chamber to the

specified pressure,

so arranging the first reactive element and the
~~second reactive element that a straight line passing~~
through a center axis of the second reactive element and a
5 straight line passing through a center axis of the first
reactive element are generally coincident with each other,

wherein the plasma is generated with the straight
line passing through the center axis of the second reactive
element and the straight line passing through the center
10 axis of the first reactive element being generally
coincident with each other.

According to a 38th aspect of the present
invention, there is provided a plasma processing method
according to the 35th aspect, comprising: before controlling
15 the interior of the vacuum chamber to the specified
pressure,

arranging the high-frequency output terminal so
as to be the other end itself of the second reactive
element,

20 wherein the plasma is generated with the high-
frequency output terminal being the other end itself of the
second reactive element.

According to a 39th aspect of the present
invention, there is provided a plasma processing method
25 according to the 35th aspect, comprising: before controlling

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~~arranging substantial distance from the other end~~
of the second reactive element to the counter electrode or
5 antenna to be not more than $1/10$ of wavelength of the high-
frequency power,

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generating the plasma by applying a high-frequency power having a frequency of 50 MHz to 300 MHz to

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According to a 42nd aspect of the present invention, there is provided a plasma processing method according to the 40th aspect, further comprising: before controlling the interior of the vacuum chamber to the specified pressure,

so arranging the first variable capacitor and the second variable capacitor that a straight line passing through a center axis of the second variable capacitor and a straight line passing through a center axis of the first variable capacitor are generally coincident with each other,

wherein the plasma is generated with the straight line passing through the center axis of the second variable capacitor and the straight line passing through the center axis of the first variable capacitor being generally coincident with each other.

According to a 43rd aspect of the present invention, there is provided a plasma processing method according to the 40th aspect, comprising: before controlling the interior of the vacuum chamber to the specified pressure,

arranging the high-frequency output terminal so as to be the other end itself of the second reactive element,

wherein the plasma is generated with the high-frequency output terminal being the other end itself of the

second variable capacitor.

According to a 44th aspect of the present invention, ~~there is provided a plasma processing method~~ according to the 40th aspect, further comprising: before
5 controlling the interior of the vacuum chamber to the specified pressure,

arranging substantial distance from the other end of the second variable capacitor to the counter electrode or antenna to be not more than $1/10$ of wavelength of the
10 high-frequency power,

wherein the plasma is generated with the substantial distance from the other end of the second variable capacitor to the counter electrode or antenna to be not more than $1/10$ of wavelength of the high-frequency
15 power.

According to a 45th aspect of the present invention, there is provided a plasma processing apparatus comprising:

- a vacuum chamber;
- 20 a gas supply unit for supplying gas into the vacuum chamber;
- an evacuating device for evacuating interior of the vacuum chamber;
- a substrate electrode for placing thereon a
25 substrate within the vacuum chamber;

a counter electrode or an antenna provided opposite to the substrate electrode;

high-frequency power supply capable of supplying
a high-frequency power having a frequency of 50 MHz to 300
5 MHz to the counter electrode or antenna;

the matching box as defined in the 30th aspect;
and

a high-frequency coupling device for connecting
the high-frequency output terminal of the matching box and
10 the counter electrode or antenna to each other,

wherein a straight line passing through a center
axis of the high-frequency coupling device, a straight line
passing through a center axis of the counter electrode or
antenna, and a straight line passing through a center axis
15 of the substrate are so arranged as to be generally
coincident together.

According to a 46th aspect of the present
invention, there is provided a plasma processing apparatus
according to the 45th aspect, wherein a straight line
20 passing through a center axis of the high-frequency output
terminal and a straight line passing through the center axis
of the high-frequency coupling device are so arranged as to
be generally coincident with each other.

According to a 47th aspect of the present
25 invention, there is provided a plasma processing apparatus

according to the 45th aspect, wherein the first reactive element and the second reactive element are so arranged that a straight line passing through a center axis of the second reactive element and a straight line passing through a center axis of the first reactive element are generally coincident with each other.

According to a 48th aspect of the present invention, there is provided a plasma processing apparatus according to the 45th aspect, wherein the high-frequency output terminal is the other end itself of the second reactive element.

According to a 49th aspect of the present invention, there is provided a plasma processing apparatus according to the 45th aspect, wherein substantial distance from the other end of the second reactive element to the counter electrode or antenna is not more than $1/10$ of wavelength of the high-frequency power.

According to a 50th aspect of the present invention, there is provided a plasma processing apparatus comprising:

a vacuum chamber;

a gas supply unit for supplying gas into the vacuum chamber;

an evacuating device for evacuating interior of the vacuum chamber;

a substrate electrode for placing thereon a substrate within the vacuum chamber;

a counter electrode or an antenna provided opposite to the substrate electrode;

5 high-frequency power supply capable of supplying a high-frequency power having a frequency of 50 MHz to 300 MHz to the counter electrode or antenna;

the matching box as defined in the 30th aspect; and

10 a high-frequency coupling device for connecting the high-frequency output terminal of the matching box and the counter electrode or antenna to each other,

wherein a straight line passing through a center axis of the high-frequency coupling device, a straight line passing through a center axis of the counter electrode or antenna, and a straight line passing through a center axis of the substrate are so arranged as to be generally coincident together.

According to a 51st aspect of the present invention, there is provided a plasma processing apparatus according to the 50th aspect, wherein the plasma is generated while the straight line passing through the center axis of the high-frequency output terminal and the straight line passing through the center axis of the high-frequency coupling device are so arranged as to be generally

coincident with each other.

According to a 52nd aspect of the present invention, there is provided a plasma processing apparatus.

5 according to the 50th aspect, wherein a first variable capacitor and a second variable capacitor are so arranged that a straight line passing through a center axis of the second variable capacitor and a straight line passing through a center axis of the first variable capacitor are generally coincident with each other.

10 According to a 53rd aspect of the present invention, there is provided a plasma processing apparatus according to the 50th aspect, wherein the high-frequency output terminal is the other end itself of the second variable capacitor.

15 According to a 54th aspect of the present invention, there is provided a plasma processing apparatus according to the 50th aspect, wherein substantial distance from the other end of the second variable capacitor to the counter electrode or antenna is not more than $1/10$ of wavelength of the high-frequency power.

BRIEF DESCRIPTION OF THE DRAWINGS

25 These and other aspects and features of the present invention will become clear from the following description taken in conjunction with the preferred embodiments thereof with reference to the accompanying

constitution of a plasma processing apparatus employed in a seventh embodiment of the present invention;

Fig. 9 is a chart showing measuring results of ion saturation current density in the seventh embodiment of the present invention;

Fig. 10 is a sectional view showing the constitution of a plasma processing apparatus employed in an eighth embodiment of the present invention;

Fig. 11 is a sectional view showing the constitution of a plasma processing apparatus employed in a ninth embodiment of the present invention;

Fig. 12 is a sectional view showing the constitution of a plasma processing apparatus employed in another embodiment of the present invention;

Fig. 13 is a sectional view showing the constitution of a plasma processing apparatus employed in another embodiment of the present invention;

Fig. 14 is a plan view of constitution of plasma traps employed in another embodiment of the present invention;

Fig. 15 is a sectional view showing the constitution of a plasma processing apparatus employed in a prior art example;

Fig. 16 is a sectional view showing the constitution of a plasma processing apparatus employed in a

Fig. 17 is a chart showing measuring results of ion saturation current density in a prior art example;

Fig. 18 is a chart showing measuring results of ion saturation current density in a prior art example;

Fig. 19 is a sectional view showing the constitution of a plasma processing apparatus employed in a tenth embodiment of the present invention;

Fig. 20 is a chart showing measuring results of ion saturation current density in the tenth embodiment of the present invention;

Fig. 21 is a sectional view showing the constitution of a plasma processing apparatus employed in an eleventh embodiment of the present invention;

Fig. 22 is a sectional view showing the constitution of a plasma processing apparatus employed in a twelfth embodiment of the present invention;

Fig. 23 is a sectional view showing the constitution of a plasma processing apparatus employed in a thirteenth embodiment of the present invention;

Fig. 24 is a sectional view showing the constitution of a plasma processing apparatus employed in a prior art example;

Fig. 25 is a chart showing measuring results of ion saturation current density in the prior art example;

Fig. 26 is a sectional view showing the constitution of a plasma processing apparatus employed in another prior art example;

Fig. 27 is a sectional view showing the constitution of a plasma processing apparatus employed in a modification of the third embodiment of the present invention;

Fig. 28 is a sectional view showing the constitution of a plasma processing apparatus employed in a modification of the eighth embodiment of the present invention;

Fig. 29 is a sectional view showing the constitution of a plasma processing apparatus where the plasma processing apparatus in the tenth embodiment of the present invention in Fig. 19 and the plasma processing apparatus in the modification of the third embodiment of the present invention in Fig. 27 are combined with each other; and

Fig. 30 is a sectional view showing the constitution of a plasma processing apparatus where the plasma processing apparatus in the eleventh embodiment of the present invention in Fig. 21 and the plasma processing apparatus in the modification of the eighth embodiment of the present invention in Fig. 28 are combined with each other.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Before the description of the present invention proceeds, it is to be noted that like parts are designated by like reference numerals throughout the accompanying drawings.

Hereinbelow, embodiments according to the present invention are described in detail with reference to the accompanying drawings.

A first embodiment of the present invention is described below with reference to Figs. 1A, 1B, and 2.

Fig. 1A shows a sectional view of a plasma processing apparatus employed in the first embodiment of the present invention. Referring to Fig. 1A, while interior of a vacuum chamber 1 is maintained to a specified pressure by introducing a specified gas from a gas supply unit 2 into the vacuum chamber 1 and simultaneously performing evacuation by a pump 3 as an evacuating device, a high-frequency power of 100 MHz is supplied to a counter electrode 5 by a counter-electrode-use-high-frequency power supply 4. Then, plasma is generated in the vacuum chamber 1, where plasma processing such as etching, deposition, and surface reforming can be carried out on a substrate 7 placed on a substrate electrode 6. A substrate-electrode-use-high-frequency power supply 8 for supplying high-frequency power to the substrate electrode 6 is also

provided, so that ion energy that reaches the substrate 7 can be controlled. Also, an annular, groove-like plasma trap 9 shown in Figs. 1A and 1B is provided opposite to the

substrate 7, making it possible to process the substrate 7 while the plasma distribution on the substrate 7 is controlled. The plasma trap 9 is provided in the counter electrode 5. Out of surfaces forming inner wall surfaces of the vacuum chamber 1 and opposing to the substrate 7, a portion 10 (cross hatched portion) surrounded by the plasma trap 9 has an area 0.8 time that of the substrate 7, as one example. Also, the groove width of the plasma trap 9 is 10 mm, and the groove depth of the plasma 9 is 15 mm, as one example. In addition, the counter electrode 5 is insulated from the vacuum chamber 1 by an insulating ring 11.

Fig. 2 shows measuring results of ion saturation current density at a position 20 mm just above the substrate 7. Conditions for plasma generation are gas type of Cl_2 and gas flow rate of 100 sccm, a pressure of 1 Pa, and a high-frequency power of 2 kW, as one example. It can be understood from Fig. 2 that the tendency that plasma would be richer in peripheral regions as shown in Fig. 17 is suppressed, and that uniform plasma is generated.

The reason why the uniformity of plasma is improved like this as compared with the plasma processing apparatus shown in Fig. 15 of the prior art example could

be considered as follows. Electromagnetic waves radiated from the counter electrode 5 are intensified by the plasma trap 9. Also, since plasma of low electron temperature

tends to cause hollow cathode discharge, high density plasma (hollow cathode discharge) is more likely to be generated by the plasma trap 9 surrounded by the solid surfaces. Accordingly, in the vacuum chamber 1, plasma density becomes the highest at the plasma trap 9, and through transport of plasma to vicinities of the substrate 7 by diffusion, uniform plasma can be obtained.

In addition, the hollow cathode discharge is as described below. Generally, because a solid surface in contact with plasma is negatively charged due to differences in thermal motion velocity between electrons and ions, DC electric fields that repel electrons from the solid surface are generated on the solid surface. In a space surrounded by solid surfaces, as in the plasma trap 9 illustrated in the first embodiment of the present invention, the probability at which electrons collide with the solid surfaces is lowered by the presence of the DC electric fields, making the life of the electrons to be prolonged. As a result, high-density plasma is generated in the plasma trap 9. Such a discharge is referred to as hollow cathode discharge.

The first embodiment of the present invention has

been described above on the case where the plasma trap 9 is provided in the counter electrode 5. In this case, however, there is a possibility that a self-bias voltage developed

to the counter electrode 5 causes high-density ions present

5 in the plasma trap 9 to collide with the counter electrode 5 at high energy so that sputtering of the counter electrode 5 may occur. The sputtering of the counter

electrode 5 may cause shortened life of the counter electrode 5 or mixing of impurities into the substrate 7,

10 thus being undesirable. This can be avoided by providing the plasma trap in portions other than the counter electrode 5. For example, the plasma trap 9 may be

provided in the insulating ring 11 as shown in a second embodiment of Fig. 3. Also, the plasma trap 9 may be

15 provided outside the insulating ring 11, that is, in a metallic upper wall 1a of the vacuum chamber 1 as shown in a third embodiment of Fig. 4. Further, also when the

plasma trap 9 is provided between the counter electrode 5 and the insulating ring 11 as shown in a fourth embodiment

20 of Fig. 5 or a fifth embodiment of Fig. 6, improvement can

be attained more or less. Furthermore, the plasma trap 9 may be provided between the upper wall 1a of the vacuum chamber 1 and the insulating ring 11 as shown in a sixth embodiment of Fig. 7.

25 In Fig. 1A, the plasma trap 9 is defined by three

faces, that is, an inner face, an upper face, and an outer face of the counter electrode 5. In Fig. 3, the plasma trap 9 is defined by three faces, that is, an inner face, an upper face, and an outer face of the insulating ring 11.

5 In Fig. 4, the plasma trap 9 is defined by three faces, that is, an inner face, an upper face, and an outer face of the upper wall 1a of the vacuum chamber 1. In Fig. 5, the plasma trap 9 is defined by an inner face of the counter electrode 5 and an upper face and an outer face of the
10 insulating ring 11. In Fig. 6, the plasma trap 9 is defined by an inner face and an upper face of the counter electrode 5 and an outer face of the insulating ring 11 and the upper wall 1a of the vacuum chamber 1. In Fig. 7, the plasma trap 9 is defined by an inner face of the insulating
15 ring 11 and an upper face and an outer face of the upper wall 1a of the vacuum chamber 1.

Next, a seventh embodiment of the present invention is described with reference to Figs. 8 and 9.

Fig. 8 shows a sectional view of a plasma
20 processing apparatus employed in the seventh embodiment of the present invention. Referring to Fig. 8, while interior of a vacuum chamber 1 is maintained to a specified pressure by introducing a specified gas from a gas supply unit 2 into the vacuum chamber 1 and simultaneously performing
25 evacuation by a pump 3 as an evacuating device, a high-

frequency power of 100 MHz is supplied to a spiral antenna 13 by an antenna-use-high-frequency power supply 12, and electromagnetic waves are radiated into the vacuum chamber

1 via a dielectric window 14 provided opposite to the
5 substrate 7 placed on the substrate electrode 6. Then, plasma is generated in the vacuum chamber 1, where plasma processing such as etching, deposition, and surface reforming can be carried out on the substrate 7. Besides, a substrate-electrode-use-high-frequency power supply 8 for
10 supplying high-frequency power to the substrate electrode 6 is provided, so that ion energy that reaches the substrate 7 can be controlled. Also, an annular, groove-like plasma trap 9 provided opposite to the substrate 7 makes it possible to process the substrate 7 while the plasma
15 distribution on the substrate 7 is controlled. The plasma trap 9 is provided in the dielectric window 14 to be defined by an inner, an upper, and an outer faces of the dielectric window 14. Out of surfaces of the vacuum chamber 1 opposing to the substrate 7, a portion 10 (cross
20 hatched portion) surrounded by the plasma trap 9 has an area 0.8 time that of the substrate 7, as one example. Also, the groove width of the plasma trap 9 is 10 mm, and the groove depth of the plasma 9 is 15 mm, as one example.

Fig. 9 shows measuring results of ion saturation
25 current density at a position 20 mm just above the

substrate 7. Conditions for plasma generation are gas type of Cl_2 , and gas flow rate of 100 sccm, a pressure of 1 Pa, and a high-frequency power of 2 kW, as one example. It can

be understood from Fig. 9 that the tendency that plasma
5 would be richer in peripheral regions as shown in Fig. 18 is suppressed, and that uniform plasma is generated.

The reason why the uniformity of plasma is improved like this as compared with the plasma processing apparatus shown in Fig. 16 of the prior art example could
10 be considered as follows. Electromagnetic waves radiated from the spiral antenna 13 are intensified by the plasma trap 9. Also, since plasma of low electron temperature tends to cause hollow cathode discharge, high density plasma (hollow cathode discharge) is more likely to be
15 generated by the plasma trap 9 surrounded by the solid surfaces. Accordingly, in the vacuum chamber 1, plasma density becomes the highest at the plasma trap 9, and through transport of plasma to vicinities of the substrate 7 by diffusion, uniform plasma can be obtained.

20 The seventh embodiment of the present invention has been described above on the case where the plasma trap 9 is provided in the dielectric window 14. However, the plasma trap 9 may also be provided outside the dielectric window 14 so as to be defined by three faces, that is, an
25 inner face, an upper face, and an outer face of the upper

wall 1a of the vacuum chamber 1 as shown in an eighth embodiment of Fig. 10. Further, the plasma trap 9 may be provided between the vacuum chamber 1 and the dielectric

window 14 so as to be defined by three faces, that is, an inner face of the dielectric window 14, an upper face and an outer face of the upper wall 1a of the vacuum chamber 1 as shown in a ninth embodiment of Fig. 11.

The foregoing embodiments of the present invention as described above are given only by way of example as part of many variations of the configuration of the vacuum chamber 1, the configuration and arrangement of the counter electrode 6 or antenna 13, the configuration and arrangement of the dielectric 14, and the configuration and arrangement of the plasma trap 9, within the application scope of the present invention. It is needless to say that the present invention may be applied in other various ways besides the examples given above. For example, whereas the foregoing embodiments have been described on the case where the counter electrode 6 is circular shaped, the counter electrode may also be formed in a polygonal, elliptical, or other shape. Also, whereas each of the foregoing cases has been that the antenna 13 is a spiral shaped, the antenna may be formed in a flat-plate, spoke, or other shape. Otherwise, the present invention may also be applied to a surface-wave plasma processing apparatus

having a cavity resonator 15, as shown in Fig. 12, where the cavity resonator 15 is regarded as an antenna. Furthermore, the present invention may be applied to a surface-wave plasma processing apparatus having a cavity resonator 15 and a slot antenna 16, as shown in Fig. 13.

The foregoing embodiments of the present invention have been described on the case where the plasma trap 9 is annular shaped. However, the plasma trap 9 may also be formed into a polygonal, elliptical, or other shape in accordance with the configuration of the substrate 7. Otherwise, the plasma trap 9 may be formed into a shape that is not a closed annular shape but a divisional, yet generally annular shape as shown by the plan view of Fig. 14. The above various kinds of the arrangement of the plasma trap 9 in Figs. 8, 10, and 11 etc. can be applied to the apparatus of Figs. 12 and 13.

Further, whereas the first or seventh embodiment of the present invention has been described on the case where a high-frequency power of 100 MHz is supplied to the counter electrode 6 or antenna 13, the frequency is not limited to this and the present invention is effective for plasma processing method and apparatus using frequencies of 50 MHz to 3 GHz.

Also, each of the first to seventh embodiments of the present invention has been described on the case where,

out of surfaces forming the inner wall surfaces of the vacuum chamber 1 and opposing the substrate 7, the area of the portion surrounded by the plasma trap 9 is 0.8 time the

area of the substrate 7. However, it is desirable that the area of this portion be 0.5 - 2.5 times the area of the substrate 7. If the area of this portion is less than 0.5 time the area of the substrate 7, it is difficult to obtain uniform plasma in vicinities of the substrate 7 even with a sufficient distance between the substrate 7 and the plasma trap 9. Also, if the area of this portion is over 2.5 times the area of the substrate 7, it is necessary to keep an extremely large distance between the substrate 7 and the plasma trap 9 in order to obtain uniform plasma in vicinities of the substrate 7. This, undesirably, would cause the apparatus to be increased in size, and excessive burden to be imposed on the pump 3 to hold the interior of the vacuum chamber 1 at a low pressure. For example, when the substrate has a diameter of 300 mm and the plasma trap has a diameter of 200 mm, the area of this portion surrounded by the plasma trap is 0.5 times the area of the substrate. When the substrate has a diameter of 300 mm and the plasma trap has a diameter of 300 mm, the area of this portion surrounded by the plasma trap is 2.5 times the area of the substrate.

Also, each of the first to seventh embodiments of

the present invention has been described on the case where the groove width of the plasma trap 9 is 10 mm. However, it is desirable that the groove width of the plasma trap 9

be within a range of 3 mm - 50 mm. If the groove width is less than 3 mm, or if over 50 mm, there is a possibility that hollow cathode discharge does not occur by the plasma trap 9.

Also, whereas the foregoing embodiments have been described on the case where the groove of the plasma trap 9 is rectangular section-shaped, the groove sectional shape may be U-shaped, V-shaped, or of a shape in combination of rectangular shape, U-shape, and V-shape.

Also, each of the first to seventh embodiments of the present invention has been described on the case where the groove depth of the plasma trap 9 is 15 mm. However, it is desirable that the groove depth of the plasma trap 9 be not less than 5 mm. If the groove depth is less than 5 mm, there is a possibility that hollow cathode discharge does not occur.

The plasma processing apparatus of the third embodiment in Figs. 4 and 10 may be applied in a case where the area surrounded by the plasma trap 9 is larger than the area of the substrate 7. In this case, it is suitable to use per-fluorocarbon gas such as CF_4 gas, C_2F_6 gas, C_4F_8 gas, C_5F_8 gas, etc. or hydro-fluorocarbon such as CHF_3 gas, CH_2F_2 ,

etc.

On the other hand, a plasma processing apparatus of a modification of the third embodiment in Fig. 27 and a plasma processing apparatus of a modification of the eighth
5 embodiment in Fig. 28 may be applied in a case where the area surrounded by the plasma trap 9 is not larger than the area of the substrate 7. In this case, it is suitable to use Boron-based gas such as HBr gas, or chlorine-based gas such as Cl_2 gas, BCl_3 gas, HCl gas etc.

10 Please note that although it is described as one example that the using gas is applied depending on the area surrounded by the plasma trap, the optimum selection of the using gas is not limited to this, but the optimum condition can be determined while referring to pressure, power, mixed
15 gas, and the like because the optimum selection of the using gas depends on the conditions such as pressure, power, mixed gas, and the like.

Also, the foregoing embodiments of the present invention have been described on the case where DC magnetic
20 fields are absent in the vacuum chamber 1. However, the present invention is also effective for cases where such large DC magnetic fields as to allow high-frequency power to penetrate into the plasma are absent, for example, a case where small DC magnetic fields on the order of several
25 tens gaussses are used for improvement in ignitability. Yet,

the present invention is particularly effective for cases where DC magnetic fields are absent in the vacuum chamber 1.

As apparent from the above description, the plasma processing method of the present invention for generating plasma within a vacuum chamber and processing a substrate placed on a substrate electrode within the vacuum chamber, the method comprises: generating the plasma by supplying a high-frequency power having a frequency of 50 MHz to 3 GHz to a counter electrode provided opposite to the substrate while interior of the vacuum chamber is controlled to a specified pressure by introducing gas into the vacuum chamber and, simultaneously therewith, evacuating the interior of the vacuum chamber; and processing the substrate by using the generated plasma while plasma distribution of the plasma on the substrate is controlled by an annular, groove-like plasma trap provided opposite to the substrate. Thus, because the substrate is processed while the plasma distribution on the substrate is controlled by the annular, groove-like plasma trap provided opposite to the substrate, uniform plasma can be generated so that the substrate can be uniformly processed.

Also, the plasma processing method of the present invention for generating plasma within a vacuum chamber and processing a substrate placed on a substrate electrode within the vacuum chamber, the method comprises: generating

the plasma by radiating electromagnetic waves into the vacuum chamber via a dielectric window provided opposite to the substrate by supplying a high-frequency power having a

frequency of 50 MHz to 3 GHz to an antenna while interior
5 of the vacuum chamber is controlled to a specified pressure by introducing gas into the vacuum chamber and, simultaneously therewith, evacuating the interior of the vacuum chamber; and processing the substrate by using the generated plasma while plasma distribution of the plasma on
10 the substrate is controlled by an annular, groove-like plasma trap provided opposite to the substrate. In this method, if the substrate is processed while the plasma distribution on the substrate is controlled by the annular, groove-like plasma trap provided opposite to the substrate,
15 uniform plasma can be generated so that the substrate can be uniformly processed.

Also, the plasma processing apparatus of the present invention comprises: a vacuum chamber; a gas supply unit for supplying gas into the vacuum chamber; an
20 evacuating device for evacuating interior of the vacuum chamber; a substrate electrode for placing thereon a substrate within the vacuum chamber; a counter electrode provided opposite to the substrate electrode; high-frequency power supply capable of supplying a high-frequency power
25 having a frequency of 50 MHz to 3 GHz to the counter

electrode; and an annular, groove-like plasma trap provided opposite to the substrate. Thus, uniform plasma can be generated so that the substrate can be uniformly processed.

Also, the plasma processing apparatus of the present invention comprises: a vacuum chamber; a gas supply unit for supplying gas into the vacuum chamber; an evacuating device for evacuating interior of the vacuum chamber; a substrate electrode for placing thereon a substrate within the vacuum chamber; a dielectric window provided opposite to the substrate electrode; an antenna for radiating electromagnetic waves into the vacuum chamber via the dielectric window; high-frequency power supply capable of supplying a high-frequency power having a frequency of 50 MHz to 3 GHz to the antenna; and an annular, groove-like plasma trap provided opposite to the substrate. Thus, uniform plasma can be generated so that the substrate can be uniformly processed.

Now, a tenth embodiment of the present invention is described below with reference to Figs. 19 and 20.

Fig. 19 shows a sectional view of a plasma processing apparatus employed in the tenth embodiment of the present invention. Referring to Fig. 19, while interior of a vacuum chamber 101 is maintained to a specified pressure by introducing a specified gas from a gas supply unit 102 into the vacuum chamber 101 and

simultaneously performing evacuation by a pump 103 as an evacuating device, a high-frequency power of 100 MHz is supplied to a counter electrode 107 by a counter-electrode-

use-high-frequency power supply 104 via a matching box 105

5 and a high-frequency coupling device (mount) 106. Then, plasma is generated in the vacuum chamber 101, where plasma processing such as etching, deposition, and surface

reforming can be carried out on a substrate 109 placed on a substrate electrode 108. A substrate-electrode-use-high-

10 frequency power supply 110 for supplying high-frequency power to the substrate electrode 108 is also provided, so that ion energy that reaches the substrate 109 can be controlled. In addition, the counter electrode 107 is insulated from the vacuum chamber 101 by an insulating ring

15 111.

The matching box 105, which is used to take impedance matching in supplying high-frequency power to the counter electrode 107 as a load, comprises a high-frequency input terminal 112, a first variable capacitor 113, a high-

20 frequency output terminal 114, a second variable capacitor 115, a first motor 116, a second motor 117, and a motor control circuit 118. One end of the first variable capacitor 113 is connected to the high-frequency input terminal 112, the other end being connected to the matching

25 box casing 105a, and one end of the second variable

capacitor 115 is connected to the high-frequency input terminal 112, the other end being connected to the high-frequency output terminal 114. Also, a straight line

forming the center axis of the second variable capacitor 115, a straight line forming the center axis of the high-frequency output terminal 114, a straight line forming the center axis of the high-frequency coupling device (mount) 106, a straight line forming the center axis of the counter electrode 107, and a straight line forming the center axis of the substrate 109 are arranged so as to be generally coincident together. Also, the first variable capacitor 113 and the second variable capacitor 115 are so arranged that the straight line forming the center axis of the second variable capacitor 115 and a straight line forming the center axis of the first variable capacitor 113 are generally coincident with each other. Further, a substantial distance 19 from the other end of the second variable capacitor 115 to the counter electrode 107 is $1/15$ (20 cm) of the wavelength (3 m) of the high-frequency power, as one example.

Fig. 20 shows results of measuring ion saturation current density at a position 20 mm just above the substrate 109. Conditions for plasma generation are gas type of Cl_2 , and gas flow rate of 100 sccm, a pressure of 2 Pa, and a high-frequency power of 1 kW, as one example.

Also, Fig. 19 shows the measuring position in Fig. 20. It can be understood from Fig. 20 that nonuniformity of plasma as shown in Fig. 25, where plasma density is higher on one side of the measuring position, cannot be seen.

5 The reason why the uniformity of plasma is improved like this as compared with the plasma processing apparatus shown in Fig. 24 of the prior art example could be considered as follows. In the case where a high-frequency power of 50 MHz or higher is used, there develops
10 a potential distribution in the counter electrode 107 under the effect of the arrangement of the second variable capacitor 115 within the matching box 105. However, in the tenth embodiment of the present invention, the potential distribution developed on the counter electrode 107 becomes
15 concentric because of the arrangement that a straight line forming the center axis of the second variable capacitor 115, a straight line forming the center axis of the high-frequency output terminal 114, a straight line forming the center axis of the high-frequency coupling device (mount)
20 106, a straight line forming the center axis of the counter electrode 107, and a straight line forming the center axis of the substrate 109 are generally coincident together. As a result, the electric fields within the vacuum chamber 101 also become concentric so that the uniformity of plasma can
25 be improved.

The foregoing tenth embodiment of the present invention has been described on the case where the counter electrode 107 is used to generate plasma. However, the present invention is also effective for cases where a spiral antenna 120 is used as in an eleventh embodiment of the present invention shown in Fig. 21. In addition, in the eleventh embodiment of the present invention shown in Fig. 21, a dielectric window 121 is used.

Also, the foregoing tenth and eleventh embodiments of the present invention are given only by way of example as part of many variations of the configuration of the vacuum chamber 101, the configuration and arrangement of the counter electrode 107 or antenna 120, the configuration and arrangement of the dielectric 121, and the like within the application scope of the present invention. It is needless to say that the present invention may be applied in other various ways besides the examples given above. For example, whereas the tenth embodiment of the present invention has been described on a case where the counter electrode 107 is circular shaped, the counter electrode may also be formed in a polygonal, elliptical, or other shape. Also, whereas the foregoing case has been that the antenna 120 is a spiral shaped, the antenna may be formed in a flat-plate, spoke, or other shape.

counter electrode 107 or antenna 120, the frequency is not limited to this and the present invention is effective for cases where frequencies of 50 MHz to 300 MHz are used. If the frequency is lower than 50 MHz, the uniformity of plasma can be easily obtained even without applying the present invention. Also, if the frequency is higher than 300 MHz, it is difficult to take impedance matching by using two variable capacitors, giving rise to a need of taking impedance matching by stubs.

Also, the tenth and eleventh embodiments of the present invention have been described on a case where the first variable capacitor and the second variable capacitor are so arranged that the straight line forming the center axis of the second variable capacitor and the straight line forming the center axis of the first variable capacitor are generally coincident with each other. However, because the potential distribution developed to the counter electrode 107 is affected primarily by the arrangement of the second variable capacitor, the uniformity of plasma is greatly improved, as compared with the prior art, also when the straight line forming the center axis of the second variable capacitor 115 and the straight line forming the

center axis of the first variable capacitor 113 are not coincident with each other as in a twelfth embodiment of the present invention shown in Fig. 22. Such a

5 where the matching box needs to be downsized, the constitution being included in the application scope of the present invention.

Also, the twelfth embodiment of the present invention has been described on the case where the matching
10 box has variable capacitors by way of example. However, the present invention produces similar effects also with a matching box having reactive elements such as variable inductors, fixed capacitors, or fixed inductors.

Also, whereas the twelfth embodiment has been
15 described on the case where the other end of the second variable capacitor 115 and the high-frequency output terminal are provided as separate members. However, the high-frequency output terminal 114 may be provided as the other end of the second variable capacitor 115 itself, as
20 in a thirteenth embodiment of the present invention shown in Fig. 23.

Also, the tenth embodiment of the present invention has been described on the case where the substantial distance from the other end of the second
25 variable capacitor 115 to the counter electrode 107 is $1/15$

of the wavelength of the high-frequency power. It is desirable that the substantial distance from the other end of the second variable capacitor 115 to the counter electrode 107 or antenna 120 be $1/10$ or less of the wavelength of the high-frequency power. If the substantial distance from the other end of the second variable capacitor 115 to the counter electrode 107 or antenna is larger than $1/10$ of the wavelength of the high-frequency power, the inductance from the other end of the second variable capacitor 115 to the counter electrode 107 or antenna becomes too large, making it difficult to take impedance matching with two variable capacitors.

In the foregoing embodiments, any one of the embodiments can be combined with any one of the embodiments. For example, Fig. 29 is a sectional view showing the constitution of a plasma processing apparatus where the plasma processing apparatus in the tenth embodiment of the present invention in Fig. 19 and the plasma processing apparatus in the modification of the third embodiment of the present invention in Fig. 27 are combined with each other. Fig. 30 is a sectional view showing the constitution of a plasma processing apparatus where the plasma processing apparatus in the eleventh embodiment of the present invention in Fig. 21 and the plasma processing apparatus in the modification of the eighth embodiment of

the present invention in Fig. 28 are combined with each other. Such a combination can obtain the both of the effects of the combined embodiments.

As apparent from the above description, the matching box of the present invention for use in a plasma processing apparatus and for taking impedance matching in supplying high-frequency power to a load, the matching box comprises: a high-frequency input terminal; a first reactive element having one end connected to the high-frequency input terminal and the other end connected to a matching box casing; a high-frequency output terminal; and a second reactive element having one end connected to the high-frequency input terminal and the other end connected to the high-frequency output terminal, wherein the second reactive element and the high-frequency output terminal are so arranged that the second reactive element is located on a straight line passing through a center axis of the high-frequency output terminal. Thus, uniform plasma can be generated so that the substrate can be uniformly processed.

Also, the matching box of the present invention for use in a plasma processing apparatus and for taking impedance matching in supplying high-frequency power to a load, the matching box comprises: a high-frequency input terminal; a first variable capacitor having one end connected to the high-frequency input terminal and the

other end connected to a matching box casing; a high-frequency output terminal; and a second variable capacitor having one end connected to the high-frequency input

terminal and the other end connected to the high-frequency
5 output terminal, wherein the second variable capacitor and the high-frequency output terminal are so arranged that the second variable capacitor is located on a straight line passing through a center axis of the high-frequency output terminal. Thus, uniform plasma can be generated so that
10 the substrate can be uniformly processed.

Also, the plasma processing method of the present invention for generating plasma within a vacuum chamber and processing a substrate placed on a substrate electrode within the vacuum chamber, the method comprises: so
15 arranging a straight line passing through a center axis of the high-frequency coupling device, a straight line passing through a center axis of the counter electrode or antenna, and a straight line passing through a center axis of the substrate as to be generally coincident together;
20 controlling interior of the vacuum chamber to a specified pressure by introducing a gas into the vacuum chamber and, simultaneously therewith, exhausting the interior of the vacuum chamber; generating the plasma by applying a high-frequency power having a frequency of 50 MHz to 300 MHz to
25 a counter electrode or antenna provided opposite to the

substrate via the matching box as defined in Claim 28 and a high-frequency coupling device provided to connect a high-frequency output terminal of the matching box and the

counter electrode or antenna to each other: and processing the substrate by using the generated plasma. Thus, uniform plasma can be generated so that the substrate can be uniformly processed.

Also, the plasma processing method of the present invention for generating plasma within a vacuum chamber and processing a substrate placed on a substrate electrode within the vacuum chamber, the method comprises: so arranging a straight line passing through a center axis of the high-frequency coupling device, a straight line passing through a center axis of the counter electrode or antenna, and a straight line passing through a center axis of the substrate as to be generally coincident together; controlling interior of the vacuum chamber to a specified pressure by introducing a gas into the vacuum chamber and, simultaneously therewith, exhausting the interior of the vacuum chamber; generating the plasma by applying a high-frequency power having a frequency of 50 MHz to 300 MHz to a counter electrode or antenna provided opposite to the substrate via the matching box as defined in Claim 33 and a high-frequency coupling device provided to connect a high-frequency output terminal of the matching box and the

counter electrode or antenna to each other; and processing the substrate by using the generated plasma. Thus, uniform plasma can be generated so that the substrate can be uniformly processed.

5 Also, the plasma processing apparatus comprises:
a vacuum chamber; a gas supply unit for supplying gas into
the vacuum chamber; an evacuating device for evacuating
interior of the vacuum chamber; a substrate electrode for
placing thereon a substrate within the vacuum chamber; a
10 counter electrode or an antenna provided opposite to the
substrate electrode; high-frequency power supply capable of
supplying a high-frequency power having a frequency of 50
MHz to 300 MHz to the counter electrode or antenna; the
matching box as defined in the 28th aspect; and a high-
15 frequency coupling device for connecting the high-frequency
output terminal of the matching box and the counter
electrode or antenna to each other, wherein a straight line
passing through a center axis of the high-frequency
coupling device, a straight line passing through a center
20 axis of the counter electrode or antenna, and a straight
line passing through a center axis of the substrate are so
arranged as to be generally coincident together. Thus,
uniform plasma can be generated so that the substrate can
be uniformly processed.

25 Also, the plasma processing apparatus comprises:

a vacuum chamber; a gas supply unit for supplying gas into the vacuum chamber; an evacuating device for evacuating interior of the vacuum chamber; a substrate electrode for placing thereon a substrate within the vacuum chamber; a counter electrode or an antenna provided opposite to the substrate electrode; high-frequency power supply capable of supplying a high-frequency power having a frequency of 50 MHz to 300 MHz to the counter electrode or antenna; the matching box as defined in the 33rd aspect; and a high-frequency coupling device for connecting the high-frequency output terminal of the matching box and the counter electrode or antenna to each other, wherein a straight line passing through a center axis of the high-frequency coupling device, a straight line passing through a center axis of the counter electrode or antenna, and a straight line passing through a center axis of the substrate are so arranged as to be generally coincident together. Thus, uniform plasma can be generated so that the substrate can be uniformly processed.

Although the present invention has been fully described in connection with the preferred embodiments thereof with reference to the accompanying drawings, it is to be noted that various changes and modifications are apparent to those skilled in the art. Such changes and modifications are to be understood as included within the

scope of the present invention as defined by the appended claims unless they depart therefrom.

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